

Coupling Tunable D-band Directional Coupler for Millimeter-wave Applications

1st Weiye Xu
Institute of Plasma Physics
Chinese Academy of Sciences
Hefei, China
xuweiye@ipp.cas.cn

2nd Handong Xu
Institute of Plasma Physics
Chinese Academy of Sciences
Hefei, China
xhd@ipp.cas.cn

3rd Fukun Liu
Institute of Plasma Physics
Chinese Academy of Sciences
Hefei, China
fklou@ipp.cas.cn

Abstract—The directional coupler is an important device for the millimeter-wave applications such as the electron cyclotron system in the magnetic confinement fusion research. A coupling tunable D-band directional coupler was designed based on a novel coupling grid structure proposed in this paper. The designed directional coupler has excellent performance with ultra-wideband. The coupling can be tuned from -28.2 dB to -33.2 dB at 140 GHz by changing the angle of the coupling grid, and the dynamic range of the coupling is about 5 dB. The return loss is smaller than -15 dB in the whole D-band from 110 GHz to 170 GHz. A 3-dB coupler using the similar coupling structure was also designed. The coupling is 3.3144 dB at the center frequency of 140 GHz.

Keywords—directional coupler, millimeter-wave, power divider, coupling tunable

I. INTRODUCTION

The electron cyclotron wave (ECW) is very important in the magnetic confinement fusion research [1]. A long pulse electron cyclotron (EC) system with a goal of 140GHz/4MW/100-1000s is being developed to meet the requirement of steady-state operation on Experimental Advanced Superconducting Tokamak (EAST) in Institute of Plasma Physics Chinese Academy of Sciences (ASIPP) [2].

Microwave directional coupler is a key microwave transmission and test device in the nuclear fusion plasma heating and in many other fields such as wireless communication, radar. Directional couplers can be implemented with a variety of transmission lines, such as rectangular waveguide, circular waveguide, stripline, microstrip line, and coaxial line. Among them, the rectangular waveguide is the most widely used transmission line suitable for transmitting waves from several GHz to several hundreds of GHz.

At present, the directional couplers suitable for waves from several GHz to several hundreds of GHz are mostly based on hole coupling [3, 4], waveguide T-Junction [5], etc. The bandwidth of the conventional design is usually small and the coupling is mostly fixed, which is inconvenient for ultra-wideband or large dynamic range applications.

In this paper, a novel ultra-wideband microwave directional coupler is proposed to remedy the defects of the conventional technology. The designed directional coupler has small return loss, good directivity, and the coupling can be tuned and the tuning range is large.

II. DIRECTIONAL COUPLER DESIGN

The designed D-band directional coupler is shown in Fig. 1. The coupler includes three parts: the WR-6 rectangular waveguides, the matching structures, and the coupling grid structure that consists of five metal strips. The matching structure is a miter bend, which is to ensure that the wide side of the waveguide stays constant. The miter bends are only used between Port 1 and Port 2, and between Port 3 and Port 4. The metal strips are made of copper-plated material. The five metal strips are distributed symmetrically and equidistantly. The distance between the centers of two adjacent metal strips is $s=0.396$ mm. All metal strips have the same thickness, which is 0.02 mm. If the five metal strips are numbered from left to right as No. 1 to No. 5. No. 1 and No. 5 have the same width, which is $d_1=0.1328$ mm. No. 2, No. 3, and No. 4 also have the same width, which is $d_2=0.0913$ mm. The coupling can be controlled by adjusting the angle of the coupling grid. The angle of the coupling grid shown in Fig. 1 is 90° or -90° . When the coupling grid rotates counterclockwise, the angle changes from -90° to 90° .

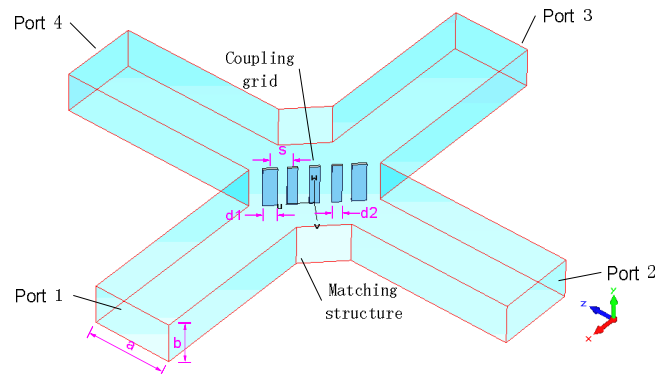


Fig. 1. Structure of the designed directional coupler. Where $a=1.651$ mm, $b=0.8255$ mm, $s=0.396$ mm, $d_1=0.1328$ mm, $d_2=0.0913$ mm.

The simulation results of the designed directional coupler are shown in Fig. 2. The return loss is smaller than -15 dB in the whole D-band from 110 GHz to 170 GHz. The insertion loss S_{21} is greater than -0.55 dB in D-band and greater than -0.15 dB at the center frequency of 140 GHz. The coupling S_{31} changes from -28.2 dB to -33.2 dB at the center frequency with the angle of the coupling grid. The dynamic range of the coupling is about 5 dB. The directivity $S_{31}-S_{41}$ is greater than 9 dB in D-band and the directivity is greater than 16 dB at the center frequency of 140 GHz.

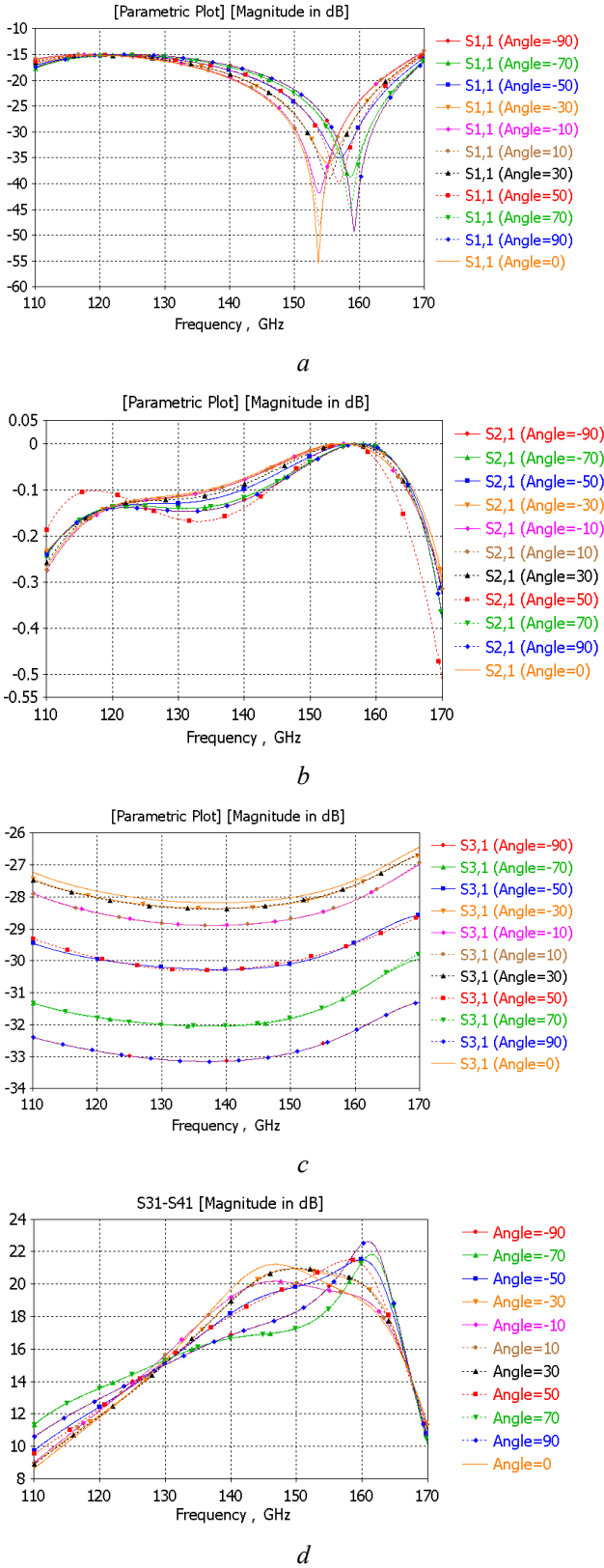


Fig. 2. Simulation results of the designed directional coupler.

- (a) Return loss, S11
- (b) Insertion loss, S21
- (c) Coupling, S31
- (d) Directivity, S31-S41.

The designed D-band directional coupler shown in Fig. 1 can be analyzed by the equivalent circuit, which is shown in Fig. 3. Where Z_1 is the equivalent impedance of the input port, which is 495 Ω .

In order to ensure the matching of the transmission line, we have,

$$\frac{1}{Z_1} = jB + \frac{1}{Z_2} + \frac{1}{Z_3} + \frac{1}{Z_4} \quad (1)$$

As can be seen from the simulation results, the coupler is nearly lossless, thus, $B=0$.

The injection power is,

$$P_{in} = \frac{1}{2} \frac{V_0^2}{Z_1} \quad (2)$$

When the angle of the coupling grid is 90° or -90° , the simulation results are as follows,

$$S_{11} = -17.13 \text{ dB} \quad (3)$$

$$S_{21} = -0.122 \text{ dB} \quad (4)$$

$$S_{31} = -33.14 \text{ dB} \quad (5)$$

$$S_{41} = -49.99 \text{ dB} \quad (6)$$

Therefore, the output power of other port is,

$$P_2 = \frac{1}{2} \frac{V_0^2}{Z_2} = 0.9723 P_{in} \quad (7)$$

$$P_3 = \frac{1}{2} \frac{V_0^2}{Z_3} = 4.853 \times 10^{-4} P_{in} \quad (8)$$

$$P_4 = \frac{1}{2} \frac{V_0^2}{Z_4} = 1.002 \times 10^{-5} P_{in} \quad (9)$$

Using the above equations, we have,

$$Z_2 = \frac{Z_1}{0.9723} = 1.028 Z_1 = 508.9 \quad (10)$$

$$Z_3 = \frac{Z_1}{4.853 \times 10^{-4}} = 2060.6 Z_1 = 1.02 \times 10^6 \quad (11)$$

$$Z_4 = \frac{Z_1}{1.002 \times 10^{-5}} = 99800 Z_1 = 4.94 \times 10^7 \quad (12)$$

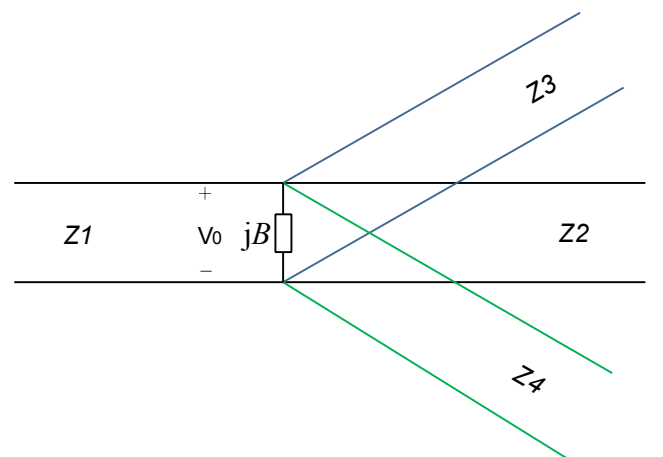


Fig. 3. The equivalent circuit for the directional coupler.

Table 1 shows the performance comparison of the proposed work with previously reported coupler in the available literature. A novel coupling method is proposed in this paper. This design has wider bandwidth, and the

coupling can be tuned by changing the angle of the coupling grid. This designed coupler is suitable for ultra-wideband and large dynamic range applications.

TABLE I PERFORMANCE COMPARISON AMONG PROPOSED AND REPORTED COUPLERS.

Ref.	Coupling method	Frequency (GHz)	Coupling (dB)	Directivity (dB)	Return loss (dB)
This work	Coupling grid	110 to 170	-28.2 to -33.2 at 140 GHz	≥ 9 in D band, >16 at 140GHz	≤ -15 in D band
[6]	Hole coupling	22 to 26	-20 at 24GHz	≥ 9 in 2 GHz range	≤ -15 in 3 GHz range
[7]	Hole coupling	26 to 40	-20 at 33GHz	≥ 9 in 10 GHz range	≤ -15 in 14 GHz range
[8]	CRLH	24.5 to 28.5	-15 at 26.5GHz	About 5	≥ -12 dB

The assembly of the directional coupler for D-band millimeter-wave applications is designed too, which is shown in Fig. 4. The flange adopts UG-387/U-M standard square flange. The flange and the metal shell are made of copper-plated material.

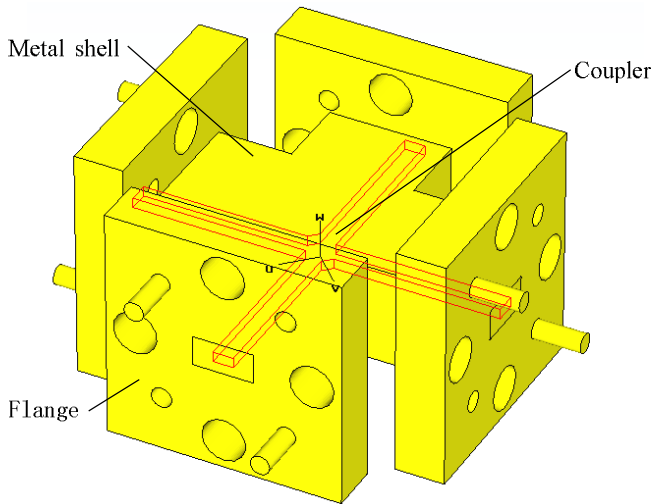


Fig. 4. Assembly of the designed directional coupler.

Actually, we can also design the directional couplers used in other bands from several GHz to several hundreds of GHz based on the coupling grid proposed in this paper. The only thing we should do is to change the size of all structures.

As shown before, the coupling can be changed by changing the angle of the coupling grid. So we design a tuning mechanism shown in Fig. 5. A putter is fixed at the edge of the metal strips, and the angle of the coupling grid can be controlled by controlling the forward or backward movement of the putter. The putter is made of dielectric materials with high hardness, such as Poly Tetra Fluoro Ethylene (PTFE). The movement of the putter can be realized manually or by using a stepper motor. When the putter moves back or forth and drives the coupling grid to rotate, it will be caused to move left or right, too. Therefore, an elongated slit needs to be formed at the

position where the putter extends out of the coupler metal shell. There are shafts at the center of the two ends of each piece of metal strip, which are inserted into the holes in the metal shell to realize the rotating support of the metal strip.

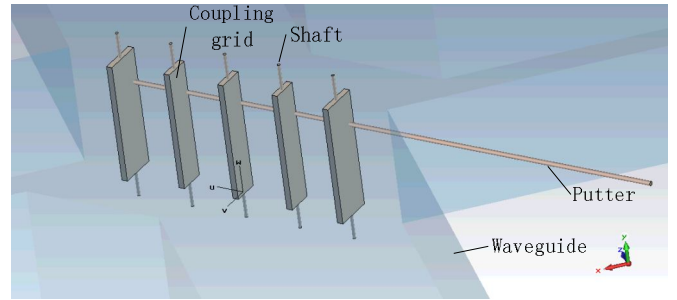


Fig. 5. Tuning structure of the designed directional coupler.

III. POWER DIVIDER (3-DB COUPLER) DESIGN

In the preceding section, a coupler with the coupling from -28.2 dB to -33.2 dB at 140 GHz is designed. Actually, we can design a 3-dB coupler use the similar coupling structure, which is shown in Fig. 6. The angle of the coupling grid is set to -60° . All metal strips have the same thickness, which is 0.02 mm.

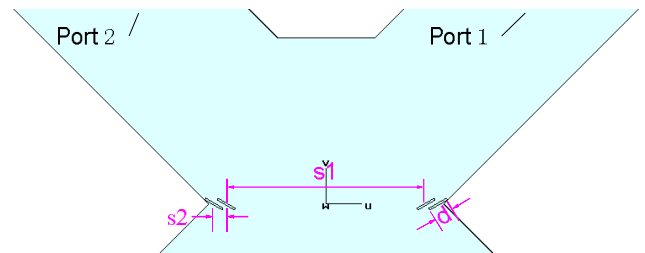


Fig. 6. Structure of the designed 3-dB directional coupler. Where $s_1=1.984$ mm, $s_2=0.12$ mm, $d=0.1$ mm.

The simulation results of the designed 3-dB coupler are shown in Fig. 7. At the center frequency of 140 GHz, $S_{21}=S_{31}=3.3144$ dB. Actually, the center frequency can be changed by changing the distance of s_1 . This design has a wider bandwidth than that reported previously in the available literature [9, 10].

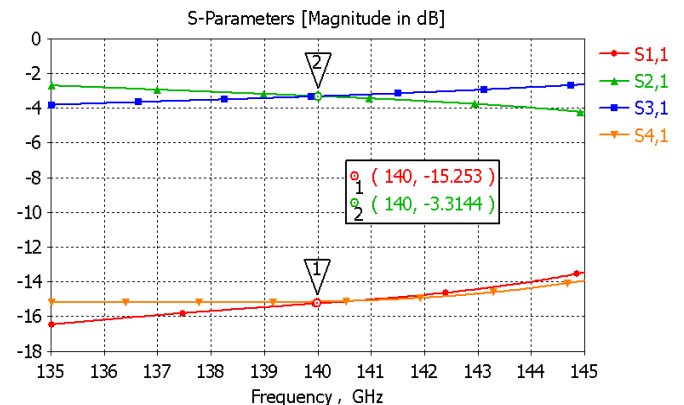


Fig. 7. Simulation results of the designed 3-dB directional coupler.

The simulation results of the power divider are as follows,

$$S_{11} = -15.25 \text{ dB} \quad (13)$$

$$S_{21} = -3.314 \text{ dB} \quad (14)$$

$$S_{31} = -3.326 \text{ dB} \quad (15)$$

$$S_{41} = -15.15 \text{ dB} \quad (16)$$

Therefore, the output power of other port is,

$$P_2 = 0.466 P_{in} \quad (17)$$

$$P_3 = 0.465 P_{in} \quad (18)$$

$$P_4 = 0.0305 P_{in} \quad (19)$$

The parameters of the equivalent circuit shown in Fig. 3 are,

$$z_2 = \frac{z_1}{0.466} = 2.146 Z_1 = 1062.3 \quad (20)$$

$$z_3 = \frac{z_1}{0.465} = 2.151 Z_1 = 1064.7 \quad (21)$$

$$z_4 = \frac{z_1}{0.0305} = 32.787 Z_1 = 1.63 \times 10^4 \quad (22)$$

These are the typical parameters of the power divider. Z_2 and Z_3 is about twice the Z_1 .

IV. CONCLUSION

A coupling tunable D-band directional coupler is designed based on a novel coupling grid structure proposed in this paper for the EC system on EAST and the other millimeter-wave applications. The designed directional coupler has excellent performance with a wider bandwidth. It is suitable for ultra-wideband or large dynamic range applications. A 3-dB coupler using the similar coupling structure is also designed. The coupling is 3.3144 dB at the center frequency of 140 GHz. Actually, the directional couplers used in other bands from several GHz to several hundreds of GHz can also be designed using the coupling grid structure proposed in this paper.

ACKNOWLEDGMENT

This work was supported in part by the National Key R&D Program of China under Grant 2017YFE0300401 and the National Magnetic Confinement Fusion Science Program of China under Grant 2015GB102003 and Grant 2015GB103000.

REFERENCES

- [1] A. W. Taylor, R. A. Cairns, and M. R. O'Brien, "Theory of High-Power Electron-Cyclotron Resonance Heating," *Plasma Physics and Controlled Fusion*, vol. 30, no. 8, pp. 1039-1057, Jul, 1988.
- [2] H. Xu, X. Wang, F. Liu, J. Zhang, Y. Huang, J. Shan, D. Wu, H. Hu, B. Li, M. Li, Y. Yang, J. Feng, W. Xu, Y. Tang, W. Wei, L. Xu, Y. Liu, H. Zhao, J. Lohr, Y. A. Gorelov, J. P. Anderson, W. Ma, Z. Wu, J. Wang, L. Zhang, F. Guo, H. Sun, X. Yan, and T. East, "Development and Preliminary Commissioning Results of a Long Pulse 140 GHz ECRH System on EAST Tokamak (Invited)," *Plasma Science and Technology*, vol. 18, no. 4, pp. 442-448, 2016.
- [3] H. A. Bethe, "Theory of Diffraction by Small Holes," *Physical Review*, vol. 66, no. 7-8, pp. 163-182, 10/01/, 1944.
- [4] S. B. Cohn, "Microwave Coupling by Large Apertures," *Proceedings of the IRE*, vol. 40, no. 6, pp. 696-699, 1952.
- [5] W. Chi, and K. A. Zaki, "Full-wave modeling of generalized double ridge waveguide T-Junctions," *IEEE Transactions on Microwave Theory and Techniques*, vol. 44, no. 12, pp. 2536-2542, 1996.
- [6] J. Guo, and K. Wu, "Variable propagation constant directional coupler," *Electronics Letters*, vol. 53, no. 6, pp. 419-421, 2017.
- [7] F. Parment, A. Ghiotto, T. P. Vuong, J. M. Duchamp, and K. Wu, "Air-to-Dielectric-Filled Two-Hole Substrate-Integrated Waveguide Directional Coupler," *IEEE Microwave and Wireless Components Letters*, vol. 27, no. 7, pp. 621-623, 2017.
- [8] G. Sajin, S. Simion, F. Craciunoiu, A. C. Bunea, A. A. Muller, and A. Dinescu, "Metamaterial millimeter wave directional coupler on silicon substrate." pp. 269-272.
- [9] W. Kong, P. Li, M. Chang, and G. Yang, "Miniaturization design of 3dB directional coupler applied to balanced power amplifier in WLAN system." pp. 571-573.
- [10] A. Taeb, M. Basha, S. Gigoyan, G. Rafi, S. Chaudhuri, and S. Safavi-Naeini, "A monolithic low-cost 3-dB directional coupler based on silicon image guide (SIG) technology at millimeter-wave band." pp. 1102-1105.